## SFH 7779 (IR-LED + Proximity Sensor + Ambient Light Sensor)

## Application Note

## 1. Introduction

The SFH 7779 combines a digital ambient light sensor and a proximity sensor (emitter + detector) within an ultra-small package. Additionally the sensor provides an  $I^2$ C-bus interface and an interrupt pin to connect it to an e.g. microcontroller.

This application note describes the basic technical features and the components operation, allowing the user to achieve the full functionality and performance of the sensor. At the end a simple software code illustrates an example for the implementation of the SFH 7779 (in the following simply abbreviated as 'SFH 7779') into a mobile phone environment.

Please note that this guide is only a brief introduction. For more detailed information and the latest products and updates please visit www.osram-os.com or contact your local sales office to get technical assistance during your design-in phase.

## 2. Applications

Typical application areas are mobile phones, PDAs, notebooks, cameras and other consumer products. Common tasks for the ambient light sensor are e.g. display adjustments. brightness whereas the proximity sensor is usually employed to detect objects and motions. This single component integrates several distinct functionalities and greatly simplifies the design-in process in consumer as well as industrial applications. The dark black look of the SFH 7779 makes it ideally suitable for implementation behind black cover glasses. Furthermore the SFH 7779 is capable of measuring the ambient light value outside the phone, even if the sensor is placed



Fig. 1: Photography and orientation of the SFH 7779.

behind a dark cover glass with different spectral transmission characteristics.

The ultra-low power consumption makes the SFH 7779 especially suited for mobile applications, where conservation of battery power is a critical point.

## 3. The SFH 7779

The SFH 7779 (see Fig. 1) consists of an 940 nm infrared (IR) LED and an ultra-low power ASIC which performs the signal processing and provides the  $I^2$ C-bus interface as well as an interrupt alert function. Additionally the ASIC contains two photodiodes: one for proximity and infra-red ambient light and another for visible ambient light sensing. The functional block diagram can be found in Fig. 2. The pinning of the device is stated in Tab. 1. The key features of the SFH 7779 include:

## Proximity Sensor (PS)

- detection-range beyond 100 mm
- optimized for the integrated 940nm emitter
- ambient light suppression
- immunity to crosstalk
- (especially for one-hole aperture designs) - improved black-hair detection

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Fig. 2: SFH 7779 functional block diagram.

Pin	Pin	Description
No.	Label	
1	V <sub>DD</sub>	Digital Supply Voltage
2	SCL	I <sup>2</sup> C-Bus Clock Line
3	GND	Ground
4	LED_A	IR-LED Anode
5	LED_C	IR-LED Cathode
6	LDR	LED Driver - connect to LED_C
7	INT	Interrupt Pin
8	SDA	I <sup>2</sup> C-Bus Data Line

Tab. 1: Pin configuration of the SFH 7779

#### Ambient Light Sensor (ALS)

- 0.002 lx 73 000 lx
- excellent linearity
- dual ALS concept (optimized to work behind dark cover glasses)
- lamp type detection

## **P**C-Bus Interface

- slave address 0x39
- 100kHz / 400kHz  $I_2C$  bus speed
- programmable operation modes (*stand-by, free-running*)
- ultra low current consumption (< 1.5 μA) in *stand-by* mode
- configurable interrupt output with programmable threshold/hysteresis levels for PS and ALS
- persistence filter for interrupt

## 4. Ambient Light Sensor

The ambient light sensor is intended to provide ambient light measurement, e.g. to control and adjust the display brightness. To support this functionality the SFH 7779 provides a convenient user interface.

The ambient light sensor module consists of two photodiodes, labelled ALS\_VIS (mainly sensitive in the visible range) and ALS\_IR (sensitive in the infrared range) with different spectral characteristics.

The true illumination resp. lux can be calculated based on the information gathered by both diodes (see Eq. (1) on next page).

The two ambient light sensors deliver output values in the range from 0 to 65535 (16 bit). Low output values correspond to a low illumination of the sensor, while high values indicate high illumination. The range of the ambient light sensor sensitivity can be set by the user and covers more than 4  $\frac{1}{2}$ decades in each setting. Two threshold the ambient light sensor levels for (ALS VIS) can be set via the I<sup>2</sup>C-bus, a lower and an upper threshold. In the case of exceeding this specified range, an interrupt signal can be generated, allowing e.g. the microcontroller to act accordingly (see Sec. 8.3 for the relevant registers and settings).

## 4.1 Spectral Sensitivity of the ALS

The spectral sensitivities of the ALS VIS and ALS IR sensor of the SFH 7779 (see Fig. 3) are designed to provide ample information about the light source and allows subsequently with a simple set of equations to calculate the true ALS value (illumination) based on this data. This is important especially as in mobile applications the SFH 7779 is often hidden behind a dark. IR-transmissive cover class. which makes it difficult for a single channel ALS to calculate the (true) ALS value.

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The following Eqs. are recommended to be applied to calculate the true ALS lux-value out of the ALS\_VIS and ALS\_IR data. The Eqs. are valid for the illumination in front of the sensor (e.g. no cover glass or glasses with flat transmission characteristics from visible into the IR region). For applications with a (dark) cover glass please refer to Sec. 10.1.

- LUX = (1.339 \* ALS\_VIS / GAIN\_VIS - 1.972 \* ALS IR / GAIN IR)
- ELSE IF (ALS\_IR/ALS\_VIS) < (0.95 \* 1.45) LUX = (0.701 \* ALS\_VIS / GAIN\_VIS - 0.483 \* ALS\_IR / GAIN\_IR)
- ELSE IF (ALS\_IR/ALS\_VIS) < (1.5 \* 1.45) LUX = (2 \* 0.701 \* ALS\_VIS / GAIN\_VIS - 1.18 \* 0.483 \* ALS\_IR / GAIN\_IR)
- ELSE IF (ALS\_IR/ALS\_VIS) < (2.5 \* 1.45) LUX = (4 \* 0.701 \* ALS\_VIS / GAIN\_VIS - 1.33 \* 0.483 \* ALS\_IR / GAIN\_IR)

```
Else
```

```
LUX = 8 * 0.701 * ALS_VIS / GAIN_VIS
```

```
LUX = LUX * 100 ms / T_INT_ALS
Eq. (1)
```

With  $\underline{\textbf{T}}_{INT}\underline{\textbf{ALS}}$  representing the ALS integration time  $(t_{INT}\underline{\textbf{ALS}})$  according to register 0x41 setting and  $\underline{\textbf{GAIN}}\underline{\textbf{VIS}} = \underline{\textbf{GAIN}}\underline{\textbf{IR}}$  according to setting in reg. 0x42. If a cover glass is used an additional gain factor needs to be added to compensate for any Fresnel loss (attenuation) due to the glass.

Fig. 4 compares the calculated illumination (lux) values and relates them to the human eye sensitivity (V-lambda, V( $\lambda$ )), assuming

the same illuminance value. The values are normalized and compared to the perception of the human eye for different light sources. The typical deviation is well within  $\pm$  20 % if above Eqs. are implemented.

## 4.2 Directivity of the ALS

The angular directivity of the SFH 7779 is presented in Fig. 5. The typ. half-angle is around  $\pm 25^{\circ}$ . This is an important point for considering the design of potential cover glass apertures (please refer to Sec. 10.5 for more details).

## 4.3 Sensitivity Range of the ALS

The sensitivity range of the ALS can be programmed the user via by the MODE CONTROL (0x41) and ALS PS CONTROL register (0x42). The illumination range scales by the GAIN and ALS integration time (t<sub>INT ALS</sub>) settings. Fig. 6 presents the ALS\_VIS signal vs. the illumination range. The graph represents the highest and lowest sensitivity range setting (valid for e.g. white LEDs or fluorescence lamps). Please refer to Tab. 2 for a listing of all the possible ALS ranges.

## 5. Proximity Sensor

The proximity sensor delivers output values within the range from 0 up to 4095 (12 bit, linear). Low output values correspond to low irradiance of the sensor, while high values indicate high irradiance. Threshold levels with or without a hysteresis for an interrupt alert can be set via the  $l^2$ C-bus (see Sec. 8.3 for the relevant registers and settings). The integrated proximity measurement operates at 940 nm.





Fig. 3: Spectral sensitivity of the two ALS sensors of the SFH 7779 (ALS\_VIS and ALS\_IR have equal gain setting).



*Fig.* 4: Typ. ambient light sensor accuracy vs. different light sources (after applying Eqs (1)).

Illumination Range	GAIN ALS_VIS	<sup>t</sup> INT_ALS
1.10lx 73321lx	1	100 ms
0.57lx 36660lx	2	100 ms
0.017lx 1146lx	64	100 ms
0.0086lx 572lx	128	100 ms
0.28lx18329lx	1	400 ms
0.14lx 9164lx	2	400 ms
0.0044lx286x	64	400 ms
0.0022lx 143lx	128	400 ms

Tab. 2: ALS sensitivity vs. GAIN ALS\_VIS resp. t<sub>INT\_ALS</sub> settings (e.g. white LED or fluorescent lamp).



Fig. 5: Directional characteristics of the ambient light (ALS) and proximity (PS) sensor.



Fig. 6: Ambient light sensor count (ALS\_VIS) vs. illumination (different gain and integration time settings). The curves represent the maximum resp. the minimum sensitivity setting.

#### 5.1 Functionality of the PS

The SFH 7779 uses a single 200 µs LED pulse. Fig. 7 illustrates the signal during a complete measurement cycle. After the measurement the proximity data are immediately available and interrupt registers are updated. Measurement repetition time in the free running mode can be selected to be 10ms, 50 ms, 100 ms or 400 ms (register 0x41). Two options are available: normal mode with single IR-LED pulse and two-pulse mode with two consecutive pulses

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Fig. 7: LED drive current and timing during one proximity measurement cycle (two options are possible: normal and two-pulse mode).

where the persistence number increases twice as fast (see Sec. 5.5). PS data, PS related interrupt and persistence are updated after every pulse.

#### **5.2 Proximity Count and Detection Range**

The maximum detection range depends – among others – on target properties like size and reflectivity and on the IR-LED pulse current. To reach a maximum detection range the recommended value for the LED drive current is 200 mA.

Fig. 8 to 10 present the proximity values vs. target distance for a 100 x 100 mm<sup>2</sup> Kodak White (90 %), Kodak Grey (18 %) and Opteka Black (~ 4 %) target (no cover glass) vs. different IR-LED currents. As indicated, the typ. maximum detection range for the SFH 7779 is in the range of beyond 100 mm (by using 200 mA LED current (Kodak White and setting a threshold level for the interrupt alert at 7 counts). As a general rule it is recommended for a robust design to set the threshold level at least up to around 7 counts above any offset level (the typ. internal offset level of the SFH 7779 is below 1 count).

Despite its crosstalk-free range the SFH 7779 features zero-distance detection. E.g. touching the sensor with a human



*Fig.* 8: *Proximity sensor signal vs. target distance and LED drive current (reflector: Kodak White, 90 %, 100 x 100 mm<sup>2</sup>).* 



*Fig.* 9: *Proximity sensor signal vs. target distance and LED drive current (reflector: Kodak Grey, 18 %, 100 x 100 mm<sup>2</sup>).* 



Fig. 10: Proximity sensor signal vs. target distance and LED drive current (reflector: Opteka Black, 4 %, 100 x 100 mm<sup>2</sup>).

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Fig. 11: Radiation characteristics of the proximity sensor LED.

finger produces enough PS counts (typ. hundreds of counts above any typical threshold setting at 200 mA IR-LED current), making the sensor capable of handling touch events (see also Sec. 10.4).

# 5.3 Radiation Characteristics of the PS-LED

Fig. 11 presents the radiation characteristics of the IR-LED. As indicated, the typ. FWHM is around 50°. This characteristic influences the design of the cover glass aperture. Please refer to Sec. 10.5 for a more detailed discussion on the cover glass aperture design.

The angular sensitivity of the proximity sensor photodiode (detector) is similar compared to the emitter's radiation characteristics (see Fig. 5).

Due to its flat-top radiation characteristics a more homogeneous irradiance of any target is achieved compared to conventional (lensed) products.

## 5.4 Crosstalk

In general, most proximity sensors are hidden behind a cover glass. However, the cover glass causes reflections which might make it difficult to operate with a fixed threshold level as the crosstalk may vary due to mechanical variations for different customer assemblies. A common and proven solution is the use of an external separator to avoid the reflections from the cover glass. However, such a separator causes additional design-in effort. Due to its design the SFH 7779 is crosstalkfor insensitive а range of typical applications. Fig. 12 presents this range as a function of cover glass thickness vs. the spacing between the bottom of the cover glass and the top of the SFH 7779 (= airgap). Typical applications where the SFH 7779 works without an external separator are e.g. 0.9 mm of a (dark) cover glass thickness and an airgap of up to 0.5 mm. Note that the crosstalk-free range depends on the actual design of the cover glass aperture. To utilize the full potential of the SFH 7779 it is recommended to use a two-hole circular aperture design at the bottom side of the cover glass (please refer to Sec. 10.5 for more details). The recommended aperture diameter is e.g.  $\emptyset \leq$ 1.8 mm for a typical airgap of < 0.5 mm. Beyond the as "crosstalk-free"-indicated area the crosstalk level might rise above 1 count (strongly dependent on the scattering properties of the ink). Typically the airgap can be extended up to 0.8 mm resulting only in a slight increase in crosstalk counts. In any case it is recommended to verify the actual design. Please note that beyond the proposed "crosstalk-free"-range the sensor works as well, but might experience a certain offset-level, dependent, among other issues, on the type of glass and mechanical variations. Please note that coloured (dark) cover glasses might cause some crosstalkoffset, depending on the type/quality of the cover glass and the surrounding IRabsorbing dark material. Experimental verification of the behaviour is mandatory here. In case an offset is present, it is recommended to set the threshold at least around 7 counts above any crosstalk offset.

In contrast to conventional products (operating at 850 nm) the SFH 7779 operates at 940 nm. Among the key

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Fig. 12: Crosstalk-free range: Cover glass thickness vs. airgap. The device is "crosstalk-free" for e.g. 1.0 mm cover glass and an airgap of 0.5 mm. To achieve optimized performance a two-hole aperture design is recommended (see Fig. 13).

**Note** that the above range is based on a crosstalk level of  $\leq$  1 count at pure glass. It is important to mention that the actual crosstalk level depends also on the properties of the dark ink. Typically the device can be operated up to 0.8 mm airgap with negligible crosstalk, i.e.  $\leq$  2 counts (depending on the quality of the dark ink).

advantages of this product is a reduction of the ink-caused crosstalk level. This level can be reduced typ. by a factor of 2 to 3 compared to conventional products. This is especially useful for designs using only a one-hole aperture design.

#### 5.5 PS Persistence Feature

The SFH 7779 features a persistence option. This helps to suppress any potential flickering of the interrupt signal in case an object / signal jitters between the two thresholds (hysteresis), i.e. this functionality smoothens out the transition between interrupt on and off.

The implemented persistence function can be activated in reg. (0x43). Only if nconsecutive measurements fulfil the threshold condition the interrupt is initiated resp. turned off (n can be set to be between



Fig. 13: Two-hole aperture design for minimum crosstalk level.

1 and 15). Please note that the two-pulse operation (accessible via MODE\_CONTROL register (0x41)) in combination with persistence allows two times faster update of the interrupt functionality instead of normal (single pulse) mode operation.

## 6. Power Consumption

The following equations give an idea on the total power consumption of the SFH 7779 during standard operation at 2.5 V.

By operating the PS in the free-running mode, the current consumption in normal operation mode (single PS pulse mode) can be approximated by the following Eq. (depending on the LED current  $I_{LED}$  and the measurement repetition time  $t_{rep PS}$ ):

$$I_{AVG_{PS}} \approx 200 \mu s \cdot \frac{(I_{LED} + 6.5 \, mA)}{t_{rep_{PS}}} + 50 \mu A$$
 Eq. (2)

The current consumption during operation of the ALS depends on the ALS integration time  $t_{int\_ALS}$  as well as the ALS repetition time  $t_{rep \ ALS}$  and can be approximated by:

$$I_{AVG\_ALS} \approx 60 \ \mu A + 130 \ \mu A \cdot \frac{t_{int\_ALS}}{t_{rep\_ALS}}$$
 Eq. (3)

Example for total PS current consumption  $(I_{LED} = 100 \text{ mA and } t_{rep\_PS} = 100 \text{ ms})$ :  $\Rightarrow I_{AVG PS} \approx 263 \text{ µA (incl. IR-LED current)}$ 

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#### I2C Bus Address of SFH 7779 0x39

Tab. 3: The  $l^2$ C-bus address of the SFH 7779.

Example for total ALS current consumption  $(t_{int\_ALS} = 100 \text{ ms and } t_{rep\_ALS} = 400 \text{ ms})$ :  $\Rightarrow I_{AVG\_ALS} \approx 92 \text{ }\mu\text{A}$ 

This compares to a stand-by current consumption of less than 1.5  $\mu A$  (typ. 0.8  $\mu A).$ 

## 7. Operating Modes

The SFH 7779 can be operated in different modes:

free-running (ALS and / or PS running alone or simultaneously): The sensor continuously measures and writes the results into the relevant registers, ready to be read via the l<sup>2</sup>C-bus interface. Optionally the interrupt alert function with the userdefined threshold levels (PS and/or ALS) will be executed if such an event takes place. *stand-by:* The initial state after power-up. The SFH 7779 is in low power mode ( $I_{DD} <$ 1.5 µA), no operations are carried out, but the device is ready to respond to l<sup>2</sup>C-bus commands.

additionally, there is the off-state: **off:** The SFH 7779 is inactive, supply current is typ. below 0.8  $\mu$ A. The SDA, SCL and INT pins are in Z-state (high impedance). All register entries are reset to their default values.

The initial start-up time is 2 ms. The typ. voltage  $V_{DD}$  to switch the SFH 7779 into the off-state is < 2.0 V. To power the SFH 7779 into the stand-by mode typ. 2.0 V are required.

## 8. I<sup>2</sup>C – Bus Communication

The *I2C-bus address* of the SFH 7779 is *0x39.* 

Mode	Bit Rate
Standard mode (Sm)	≤ 100 kbit/s
Fast mode (Fm)	$\leq$ 400 kbit/s

*Tab. 4: The l*<sup>2</sup>*C-bus protocol speed mode compatibility of the SFH 7779.* 

## 8.1 I<sup>2</sup>C - Bus Environment

The SFH 7779 is a digital ambient light and proximity sensor. The communication is performed via a 2-wire I<sup>2</sup>C bus interface, so the device can be integrated into a typical / multi-slave I<sup>2</sup>C multi-master bus environment. A typical I<sup>2</sup>C bus network consists of a master and different I<sup>2</sup>C bus slave devices. For a more detailed discussion on the topic of l<sup>2</sup>C-bus please refer to [2]. The built-in I<sup>2</sup>C-bus interface is compatible

with all common  $I^2$ C-bus interface is compatible 4). The logic voltage (V<sub>IO</sub>) of the SFH 7779 ranges from 1.65 V – 3.6 V (according to  $I^2$ C-bus specification [2]).

## 8.2 I<sup>2</sup>C - Bus Communication

By embedding the SFH 7779 in an l<sup>2</sup>C-bus network and after applying  $V_{DD}$  = 2.5 V, the communication can start as follows (Fig. 14 illustrates this l<sup>2</sup>C-bus conversation):

## 1. Activation of the ALS and PS:

The default mode of the sensor is STAND-BY and the SFH 7779 needs to be activated by the master (e.g. microcontroller).

Each I<sup>2</sup>C bus communication begins with a start command "S" of the Master (SDA line is changing from "1" to "0" during SCL line stays "1") followed by the address of the slave (0x39). After the 7bit slave address the read (1) or write (0) R/W bit of the master will follow. The R/W bit controls the communication direction between the master and the addressed slave. The slave is responding to a proper communication acknowledge command. with an Acknowledge "A" (or not acknowledge "NA")

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1.1 Activate ALS (T	$^{-}$ int ALS = 100 ms.	T rep ALS = 400 ms)	and PS (T rep PS = $100 \text{ ms}$ )

1.1 Activate ALS (T_int_AL	S = 100	ms, T_rep_ALS = 400	ms) and F	PS (T_rep_PS = 100	ms)
S SFH7779 Address (0x39)	WA	Mode_Control Register (0x41)	A Act	ivate ALS + PS Mode (0x09)	A P
1.2 Set Proximity LED Curr	ent to 20	0 mA and ALS Gain to	64		
S SFH7779 Address (0x39)	WA	ALS_PS_Control Register (0x42)	A AL Curr	.S Gain + LED ent Mode (0x2B)	A P
2. Sensor in Operation 3.1 Read Out PS Data (LSI	B)				
S SFH7779 Address (0x39)	WA	PS Data Register (0x44)	AP		
S SFH7779 Address (0x39)	RA	PS Data (LSB)	A P		
3.2 Read Out PS Data (MS	B)				
S SFH7779 Address (0x39)	WA	PS Data Register (0x45)	AP		
S SFH7779 Address (0x39)	RA	PS Data (MSB)	A P		
4.1 Read Out ALS_VIS Dat	ta (LSB)				
S SFH7779 Address (0x39)	WA	ALS Data Registe (0x46)	<sup>r</sup> A P		
S SFH7779 Address (0x39)	R A	ALS Data (LSB)	A P		
4.2 Read Out ALS_VIS Dat	ta (MSB)	)			
S SFH7779 Address (0x39)	WA	ALS Data Registe (0x47)	r A P		
S SFH7779 Address (0x39)	R A	ALS Data (MSB)	A P		
4.3 Read Out ALS_IR Data	(LSB)				
S SFH7779 Address (0x39)	WA	ALS Data Registe (0x48)	r A P		
S SFH7779 Address (0x39)	RA	ALS Data (LSB)	A P		
4.4 Read Out ALS_IR Data	(MSB)				
S SFH7779 Address (0x39)	WA	ALS Data Registe (0x49)	r A P	W: Master Write	es
S SFH7779 Address (0x39)	RA	ALS Data (MSB)	A P	R: Master Read A: Acknowledge	ds e
	ation fr	om Master to SFH	7779	NA: Not Acknow S: Start Conditi	wledge on on
	ation fr	om SFH 7779 to M	aster	* this line is opt	ional

*Fig.* 14: *I*<sup>2</sup>C-bus communication for the example described below.

is performed from the receiver by pulling the SDA line down (or leave in "1" state).

For the activation of the sensor the master needs to write an activation command (e.g. 0x09 to activate ALS and the PS with T\_int\_ALS = 100 ms and repetition time of 400 ms and 100 ms for the PS) into the

corresponding mode\_control register (0x41). Each command needs to be acknowledged by the slave. After activation the master ends the communication with a STOP command "P" (SDA line is changing from LOW to HIGH during SCL line stays HIGH). Additionally the ALS gain is set to 64 and

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Fig. 15: Combined mode structure.

PS current to 200 mA by writing 0x2B into the ALS\_PS\_Control register (0x42).

#### 2. Sensor in Operation:

After activation, the sensor will change from STAND-BY to FREE-RUNNING mode. After a delay of e.g. 100 ms (depending on t<sub>INT\_ALS</sub> setting) the first measurement values are available and can be read via the I<sup>2</sup>C-bus.

#### 3. PS value: reading data (LSB and MSB)

The two byte PS value is accessible via the output registers (0x44 (LSB) and 0x45 (MSB)). After reading the two 8-bit words, the communication can be ended by the master with a not acknowledge "NA" and the stop command "P". The two byte PS output readings of the SFH 7779 can then be converted to a final decimal PS value via Eq. (4):

#### $DATA_{16bit, decimal} = DATA_{LSB} + 256 \cdot DATA_{MSB}$ Eq. (4)

#### 4. ALS value: reading data (LSB and MSB)

The sensor's two 16bit ALS measurement values are composed of 2 bytes each (LSB & MSB). The bytes are accessible via the two output registers (0x46 to 0x49). After addressing the LSB (least significant byte) resp. the MSB (most significant byte) output register, the communication direction has got to be changed from the slave to the master by repeating the address and the R/W byte with a changed R/W bit. After reading LSB and MSB, the communication is ended by the master with a not acknowledge "NA" and the stop condition

"P". The conversion of the two byte output data into 16bit values can easily be done by again using Eq. (4).

Finally the true lux value can be obtained from the two ALS data (ALS\_VIS, ALS\_IR) by using the simple instructions according to Eq. (1).

After finishing the measurement, the SFH 7779 mode may be changed to STAND-BY via the mode\_control register.

#### Combined mode

To ensure interference free communication the l<sup>2</sup>C-bus combined mode should be used. Instead of performing two independent read or write commands (COM 1 & COM 2) the commands can be combined by a repeated start condition "Sr" (Fig. 15 illustrates the combined mode structure).

The start and repeated start commands ("Sr") are the same: the SDA line is changing from "1" to "0" during SCL line "1". The "Sr" condition is placed behind "A" or "NA". The combined mode is not limited to 2 read/write commands, so the addressing of the sensor and reading/writing of multiple register values can be performed within one block.

#### Block read/write mode

The Block read/write mode of the SFH 7779 can be used to read all output registers in cyclic manner.

After addressing and reading an output register (e.g. LSB) in normal mode, the master is not placing the stop condition, but sends an acknowledge and continues to read the output registers. The SFH 7779 will automatically increase the register address and the content of the next sensor output register can be read following the register addresses:

0x40→0x41→...→0x51→0x52→0x40→...

For register addresses and content see Sec. 8.3 and Tab. 5.

The block read mode can be ended by placing a not acknowledge (NA) with the subsequent stop condition from the master.

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I <sup>2</sup> C Addr	Туре	Name	Description
0x40	R/W	SYSTEM_CONTROL	System Control
0x41	R/W	MODE_CONTROL	ALS, PS General Control
0x42	R/W	ALS_PS_CONTROL	ALS Gain and PS Current Control
0x43	R/W	PERSISTENCE	PS Interrupt Persistence Control
0x44	R	PS_DATA_LSB	LSB data for PS
0x45	R	PS_DATA_MSB	MSB data for PS
0x46	R	ALS_VIS_DATA_LSB	LSB data for ALS VIS - diode
0x47	R	ALS_VIS_DATA_MSB	MSB data for ALS VIS - diode
0x48	R	ALS_IR_DATA_LSB	LSB data for ALS IR - diode
0x49	R	ALS_IR_DATA_MSB	MSB data for ALS IR - diode
0x4A	R/W	INTERRUPT_CONTROL	Interrupt Control
0x4B	R/W	PS_TH_LSB	PS interrupt up threshold level, LSB
0x4C	R/W	PS_TH_MSB	PS interrupt up threshold level, MSB
0x4D	R/W	PS_TL_LSB	PS interrupt low threshold level, LSB
0x4E	R/W	PS_TL_MSB	PS interrupt low threshold level, MSB
0x4F	R/W	ALS_VIS_TH_LSB	ALS (VIS) interrupt up threshold level, LSB
0x50	R/W	ALS_VIS_TH_MSB	ALS (VIS) interrupt up threshold level, MSB
0x51	R/W	ALS_VIS_TL_LSB	ALS (VIS) interrupt low threshold level, LSB
0x52	R/W	ALS_VIS_TL_MSB	ALS (VIS) interrupt low threshold level, MSB

Tab. 5: SFH 7779 control and data registers.

## 8.3 Registers

The SFH 7779 has 19 different registers (see Tab. 5).

The following pages will describe the registers and their structure resp. content.

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**SYSTEM\_CONTROL:** The SYSTEM\_CONTROL register is used to control the software (SW) reset and the interrupt function (INT). Manufacturer ID and Part ID can be read.

RW-Reg	jist	er 0x40								
Bit		7		6	5	4	3	2	1	0
		SW reset		INT reset	Manufacturer ID			Part ID		
					(read only)			(read only)		
default	0	Initial rest is not started	0	INT pin status is not					001	
				initialized						
	1	Initial reset started	1	INT pin become inactive						
				(high impedance)		001				

**MODE\_CONTROL:** Mode CONTROL for PS operating modes and time settings. Normal ALS measurement time is 100 ms. High sensitive ALS mode is with a true measurement time of 400 ms (= $t_{int\_ALS}$ ). The 50 ms ALS integration time setting (1100) might lead to susceptibility to flicker and requires additional functionality in the software. This setting is not recommended by OSRAM OS.

RW-Reg	gistei	r 0x4	1				<u>.</u>
Bit	7	6	5	4	3	2	1 0
	Re	serv	ed	PS Mode		Measurement Repeti	tion Rate
	(re	ad oi	nly)			ALS	PS
default				0 normal	0000	standby	standby
	1			1 two-pulse mode	0001	standby	10 ms
					0010	standby	40 ms
					0011	standby	100 ms
					0100	standby	400 ms
					0101	100 ms (=t <sub>int ALS</sub> )	standby
					0110	100 ms (=t <sub>int ALS</sub> )	100 ms
					0111	100 ms (=t <sub>int_ALS</sub> )	400 ms
					1000	400 ms (t <sub>int ALS</sub> = 100ms	s) standby
					1001	400 ms (t <sub>int ALS</sub> = 100ms	s) 100 ms
					1010	400 ms (=t <sub>int ALS</sub> )	standby
					1011	400 ms (=t <sub>int ALS</sub> )	400 ms
	1				1100	50 ms (=t <sub>int_ALS</sub> ) *)	50 ms
					else	forbi	dden

\*) to apply the 50 ms setting the following software handling of the ALS data is necessary before lux calculation can be performed (as bit # (15) indicates data overflow in 50 ms mode). Note that the max. count in 50 ms is 0x7FFF (15 bit long instead of 16): If (ALS\_VIS & 0x8000) == 0x8000 // bitwise AND to identify the overflow flag in bit 15 of ALS\_VIS {ALS\_VIS = 0x7FFF:}

If (ALS\_VIS & 0x8000) == 0x8000 // bitwise AND to identify the overflow flag in bit 15 of ALS\_VIS
 {ALS\_VIS = 0x7FFF;}
If (ALS\_IR & 0x8000) == 0x8000 // bitwise AND to identify the overflow flag in bit 15 of ALS\_IR
 {ALS\_IR = 0x7FFF;}

R/W-R	egister 0x42	i		1	+			i
Bit	7	6	5	0				
	Reserved	PS Output	ALS	Gain fo	or ALS VIS and	I ALS IR	L	ED Current
	(read only)							
	Field	Bits	Default			Descri	ption	
Reser	ved	7	0	0	Write 0			
PS Ou	tput	6	0	0	Proximity out	put		
				1	Infrared DC lev	vel output		
ALS G	ain	5:2	0000	0000	ALS VIS: x 1	ALS IR: x 1		
				0100	ALS VIS: x 2	ALS IR: x 1		
				0101	ALS VIS: x 2	ALS IR: x 2		
				1010	ALS VIS: x 64	ALS IR: x 6	4	
				1110	ALS VIS: x 128	8 ALS IR: x 6	4	
				1111	ALS VIS: x 128	8 ALS IR: x 1	28	
				else	forbidden			
LED C	urrent	1:0	11	11	200 mA			
				00	25 mA			
				01	50 mA			
				10	100 mA			

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#### PERSISTANCE: Settings of persistence interrupt function and interrupt status.

RW-Reg	gister Ox	43						
Bit	7	6	5	4	3	2	1	0
	tence							
default		00	00		0001	Interrupt statu measurement	is updated aft	er each
					0000	Interrupt becon measurement	nes active after	reach
					0001	Interrupt status measurement	updated after	each
					0010	Interrupt status consecutive the same	is updated if to reshold judgem	wo nent are the
					0011 or higher	Interrupt status judgement are times (n is set i	is updated if the same over in bits (0:3))	hreshold n-consecutive

PS\_DATA\_LSB: LSB of the PS output.

R-Register 0x44											
Bit	7	6	5	4	3	2	1	0			
	LSB data										
default		0000 0000									

**PS\_DATA\_MSB:** MSB of the PS output.

R-Register 0x45											
Bit	7	6	5	4	3	2	1	0			
		MSB data									
default	0000 0000										

ALS\_VIS\_DATA\_LSB: LSB of the ALS VIS output.

R-Register 0x46											
Bit	7	6	5	4	3	2	1	0			
				LSB	data						
default				0000	0000						

ALS\_VIS\_DATA\_MSB: MSB of the ALS VIS output.

R-Register 0x47											
Bit	7	6	5	4	3	2	1	0			
		MSB data									
default		0000 0000									

ALS\_IR\_DATA\_LSB: LSB of the ALS IR output.

R-Register 0x48											
Bit	7 6 5 4 3 2 1 0										
	LSB data										
default	0000 0000										

ALS\_IR\_DATA\_MSB: MSB of the ALS IR output.

R-Register 0x49											
Bit	7	6	5	4	3	2	1	0			
		MSB data									
default		0000 0000									

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#### INTERRUPT CONTROL: Setting of the interrupt functions.

D /1 A	/ D		A
	/-Ke(	lister	UX4A
		,	•

Bit	7	6	5	4	3	2	1	0		
	PS INT Status	ALS INT Status	INT	Mode	INT assert	INT latch		INT trigger		
	(read only)	(read only)								
	Field	Bits	Default			Descrip	tion			
PS INT	l status	7	0	0	0 PS interrupt signal inactive					
				1 PS interrupt signal active						
ALS IN	IT status	6	0	0 ALS VIS interrupt signal inactive						
				1 ALS VIS interrupt signal active						
INT m	ode	5:4	00	00 00 PS_TH is only active						
			01	PS_TH & PS TL	are active (H	lysteresis	)			
				10	PS_TH & PS TL	are active a	s outside	detection		
				11	forbidden					
INT as	sert	3	0	0	INT "L" is stable	e if newer m	easurem	ent results is also		
					interrupt active					
				0	INT "L" is de-ass	ert and re-as	ssert if nev	ver measurement		
					results is also int	errupt active				
INT lat	ch	2	0	0	INT is latched u	ntil INT regi	ster is re	ad or initialized		
				1	INT is updated at	fter each me	asuremer	nt		
Interru	ıpt mode	1:0	00	00	INT pin is inacti	ve				
				00	) Triggered by PS only					
				10	Triggered by ALS	S VIS only				
				11	Triggered by PS	or ALS only				

Note: Bits 6 & 7 (interrupt inactive / active) are reset as soon as register 0x4A is read. This is also valid for the INT-pin (becomes inactive as soon as register 0x4A is read).

**PS\_TH\_LSB:** LSB for the PS threshold "HIGH".

RW-Register 0x4B												
Bit	7	6	5	4	3	2	1	0				
		LSB data (upper threshold)										
default				1111	1111							

PS\_TH\_MSB: MSB for the PS threshold "HIGH".

RW-Register 0x4C											
Bit	7	6	5	4	3	2	1	0			
		MSB data (upper threshold)									
default				1111	1111						

**PS\_TL\_LSB:** LSB for the PS threshold "LOW".

RW-Register 0x4D												
Bit	7	6	5	4	3	2	1	0				
		LSB data (lower threshold)										
default		0000 0000										

**PS\_TL\_MSB:** MSB for the PS threshold "LOW".

RW-Register 0x4E											
Bit	7	6	5	4	3	2	1	0			
		MSB data (lower threshold)									
default				0000	0000						

ALS\_VIS\_TH\_LSB: LSB for the ALS\_VIS threshold "HIGH".

RW-Register 0x4F												
Bit	7	6	5	4	3	2	1	0				
		LSB data (upper threshold)										
default		1111 1111										

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1

ALS\_VIS\_TH\_MSB: MSB for the ALS\_VIS threshold "HIGH".

RW-Register 0x50								
Bit	7 6 5 4 3 2 1 0							
	MSB data (upper threshold)							
default	1111 1111							

ALS\_VIS\_TL\_LSB: LSB for the ALS\_VIS threshold "LOW".

RW-Register 0x51								
Bit	7 6 5 4 3 2 1 0							
	LSB data (lower threshold)							
default	0000 0000							

ALS\_VIS\_TL\_MSB: MSB for the ALS\_VIS threshold "LOW".

RW-Register 0x52								
Bit	7 6 5 4 3 2 1 0							
	MSB data lower threshold)							
default	0000 0000							

## 9. Interrupt Alert

The SFH 7779 provides an interrupt pin which can be configured completely by the user (access via register 0x4A). E.g. the interrupt function can be configured to operate in latched or normal mode. In normal mode the interrupt event/signal is updated after every measurement, whereas in the latched mode it is guaranteed that even single peaks are detected (e.g. the interrupt is held the as long as microcontroller reads out the interrupt register). Other options include the selection of the interrupt trigger source (PS or/and ALS) as well as the option of having PS

hysteresis (e.g. in combination with a persistence function) and/or an ALS\_VIS event window (upper and lower ALS VIS threshold). For the exact interrupt event definition please refer to Tab. 6. This is especially valuable as it allows the SFH 7779 to operate as stand alone device in the free-running mode, independent from the main microcontroller. This functionality relieves the microcontroller from active involvement in the PS / ALS monitoring resp. measurement cycle and reduces significantly the I<sup>2</sup>C-bus traffic, thus reducing the overall power consumption of the system. Only if the user-defined thresholds are violated, the interrupt signal will inform

Interrupt Event Definition						
proximity sensor	Without Hysteresis:					
	ON:	PS data > PS_TH (threshold high)				
	OFF:	PS data < PS_TH (threshold high)				
	With H	With Hysteresis:				
	ON:	PS data > PS_TH (threshold high)				
	OFF:	PS data < PS_TL (threshold low)				
	Interval:					
ambient light sensor	ON:	ALS_VIS > ALS_VIS_TH (threshold high)				
ambient light senser		or				
		ALS_VIS < ALS_VIS_TL (threshold low)				
	OFF:	ALS_VIS_TL < ALS_VIS < ALS_VIS_TH				

Tab. 6: Interrupt event definition. Note that the on/off definition of the PS can be inverted by user setting within register (0x4A) to allow switching from inside target to outside target detection.

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the microcontroller and the predefined actions can be executed (e.g. after optional read-out of the interrupt and PS / ALS data registers to get the actual data - if desired).

**Note:** Interrupt pin level and bits 6 & 7 of register 0x4A (Interrupt register) are reset as soon as interrupt register 0x4A is read.

## 10 Design-in Guidelines

By implementing the SFH 7779 behind a (dark) cover glass, three issues need to be taken into account:

- ALS: ambient light calculation
- PS: maximum detection distance
- ALS & PS: aperture design

The following sections deal with these issues and give the designer valuable guidelines to achieve the maximum performance of the sensor.

#### 10.1 Implementing the Illumination (Lux) Calculation: General Procedure

The design of the sensor allows computing from the two ALS data sets (ALS\_VIS and ALS\_IR) the "true" ALS value in front of a ("dark") cover glass.

In general the calculation of the lux value is based on a set of equations which are typically derived by measurements and some mathematics. This set of equations looks like:

IF (ALS_IR / ALS_VIS) < r_0 LUX = (a_0 * ALS_VIS / GAIN_VIS - b_0 * ALS_IR / GAIN_IR)
ELSE IF (ALS_IR / ALS_VIS) < r_1 LUX = (a_1 * ALS_VIS / GAIN_VIS - b_1 * ALS_IR / GAIN_IR )
ELSE IF (ALS_IR / ALS_VIS) < r_2 LUX = (a_2 * ALS_VIS / GAIN_VIS - b_2 * ALS_IR / GAIN_IR )

ELSE IF (ALS\_IR / ALS\_VIS) < (0.95\* r\_3)

```
LUX = (a_3 * ALS_VIS / GAIN_VIS

- b_3 * ALS_IR / GAIN_IR )

ELSE IF (ALS_IR/ALS_VIS) < (1.5 * r_3)

LUX = (2 * a_3 * ALS_VIS / GAIN_VIS

- 1.18 * b_3 * ALS_IR / GAIN_IR)

ELSE IF (ALS_IR/ALS_VIS) < (2.5 * r_3)

LUX = (4 * a_3 * ALS_VIS / GAIN_VIS

- 1.33 * b_3 * ALS_IR / GAIN_IR)

ELSE

LUX = (8 * a_3 * ALS_VIS / GAIN_VIS)

LUX = LUX * 100 ms / T_INT_ALS

Eq. (5)
```

The first case (indicated by  $ALS_IR / ALS_VIS < r_0$ ) covers e.g. LED, fluorescence and sunlight based lighting situations. The second case (<  $r_1$ ) handles incandescent and halogen lamps, whereas cases three (<  $r_2$ ) and four (<  $0.95 \cdot r_3$ ) cover dimmed halogen and incandescence lamps, characterized by increased IR content.

The following cases (<  $(1.5 \cdot r_3)$  and <  $(2.5 \cdot r_3)$ ) need always to be added as the final ELSE IF condition to compensate for titled situations and relate to the last constants (in this case to  $r_3$ ,  $a_3$  and  $b_3$ ). The same holds true for the final ELSE statement ( $a_3$  always relates to the constant a of the last ELSE IF statement).

The way to obtain the parameters of the equations is governed by four steps:

- 1) measurement under different lighting conditions
- 2) harmonization of results and plotting
- 3) grouping and linear approximation
- 4) derive set of final equations for illumination calculation

In the following pages this procedure is described in more detail:

1) Based on a setup according to Fig. 16 the illumination value  $E_{v\_Measured}$  (in lux) in front of the cover is recorded in parallel to the

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Fig. 16: Measurement setup for deriving the required equations to calculate the illumination (lux) value out of ALS\_VIS, ALS IR.

readings of ALS\_VIS resp. ALS\_IR (with appropriate settings of ALS gain to avoid saturation resp. too low counts); see Tab. 7. This needs to be performed with various different light sources

For best results it is recommended that the light source dimension d is small compared to  $\triangle d$ , the distance light source – SFH 7779. Recommended is  $\triangle d/d > 6$ . If this can not be

achieved a mechanical aperture in the optical path is recommended.

2) The next step comprises a harmonization of the results, considering normalizing all obtained data to the same ALS gain setting resp.  $t_{INT\_ALS}$  setting (100 ms or 400 ms). A recommended approach is to normalize all measurements to e.g. 100 ms, unity gain (GAIN ALS\_VIS = GAIN ALS\_IR = 1) and to identical illumination value  $E_{v\_norm}$  (e.g. 1 lux).

In essence it means to normalize the measured ALS\_VIS and ALS\_IR data (see also Tab. 7) by using:

$$ALS \_VIS = \frac{ALS_{VIS}\_MEASURED}{E_{v\_Measured}(in lux)} \cdot \frac{100 ms}{t_{INT}\_ALS} \cdot GAIN_{VIS}$$
Eq. (6)
$$ALS \_IR = \frac{ALS_{IR}\_MEASURED}{E_{v\_Measured}(in lux)} \cdot \frac{100 ms}{t_{INT}\_ALS} \cdot GAIN_{IR}$$
Eq. (7)

The obtained data points from Eqs. (6) and (7) are now plotted into a diagram (ALS\_IR vs. ALS\_VIS) like in Fig. 17.

3) The next step is to group the data points together like seen in Fig. 17 and derive the linear approximation equation for each group. Recommended grouping linearization could combine light sources with similar properties, e.g. combine white LEDs and fluorescence lamps. Next group could and be halogen traditional incandescent lamps. The final group(s) could be dimmed incandescent light sources as their IR/VIS ratio is the highest.

	Fluorescence Lamp	White LED	Halogen Lamp	Incand. Lamp	Dimmed Incand. Lamp	Dimmed Halogen Lamp	Sunlight
Illumination in Front							
of Cover / lux	215	6750	245	185	118	26	100000
Gain Setting	64	2	64	2	2	128	1
ALS_VIS_measured	1320	1500	9200	425	970	3400	28000
ALS_IR_measured	65	35	7700	360	1360	2700	15000
	$\downarrow$ $\downarrow$ $\downarrow$ via Eqs. (6) and (7) $\downarrow$ $\downarrow$					$\downarrow$	
ALS_VIS *)	0.096	0.111	0.587	1.149	4.110	1.022	0.280
ALS_IR *)	0.005	0.003	0.491	0.973	5.763	0.811	0.150
ALS_IR / ALS_VIS							
Ratio	0.049	0.023	0.837	0.847	1.402	0.794	0.536

Tab. 7: Example of measured ALS data for various light sources and their normalized values (measured with a cover glass transmission acc. to Fig. 18). \*) normalized to 1 lux and gain = 1.

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Fig. 17: Graph representing the normalized ALS data points (according to Eq. (6) and (7)). The linear approximation is done here with e.g. three linear segments and corresponds to a cover glass according to Fig. 18. Inset: Zoomed area at low ALS data.

The mathematical syntax is as follows for the linear approximation (resulting in N+1 equations):

Group 0:  $ALS_{IR} = c_0 \cdot ALS_{VIS} - d_0$ Group 1:  $ALS_{IR} = c_1 \cdot ALS_{VIS} - d_1$ 

Group N:  $ALS_{IR} = c_N \cdot ALS_{VIS} - d_N$ Eq. (8)

4) Now the linearization Eqs. (8) are compared with the original illumination (lux) Eqs. to derive the constant values:

Group 0:  $LUX = a_0 \cdot ALS \_VIS - b_0 \cdot ALS \_IR$ Group 1:  $LUX = a_1 \cdot ALS \_VIS - b_1 \cdot ALS \_IR$ .... Group N:  $LUX = a_N \cdot ALS \_VIS - b_N \cdot ALS \_IR$ Eq. (9) The two sets of equations (8 and 9) can be solved to determine the constant values  $a_{x}$  resp.  $b_{x}$ . The result is as follows with  $E_{v\_norm}$  as the normalized illumination in lux (i.e.  $E_{v\_norm} = 1$  lx; according to step 3).

$$a_i = E_{v_norm} \cdot c_i / d_i \qquad \qquad \text{Eq. (10)}$$

$$b_i = E_{v_norm} / d_i \qquad \qquad \text{Eq. (11)}$$

The constant values (a, b) in Eqs. (9) are now determined. The last step is to define the threshold level  $\mathbf{r}_{_{N}}$  at which point one equation is replaced by the next one:

$$r_{0} = \frac{ALS \_IR}{ALS \_VIS} = \frac{(a_{0} - a_{1})}{(b_{0} - b_{1})}$$

$$r_{1} = \frac{ALS \_IR}{ALS \_VIS} = \frac{(a_{1} - a_{2})}{(b_{1} - b_{2})}$$
...
$$r_{N} = \frac{ALS \_IR}{ALS \_VIS} = \frac{(a_{N} - 0)}{(b_{N} - 0)}$$
Eq. (12)

The final instruction set for implementation now need to take again into account any different settings (gain, t<sub>INT\_ALS</sub>) under which the sensor is operated and look like:

```
IF (ALS IR / ALS VIS) < r 0
   LUX = (a_0 * ALS_VIS / GAIN_VIS
          - b_0 * ALS_IR / GAIN_IR)
ELSE IF (ALS_IR / ALS_VIS) < r_1
LUX = (a_1 * ALS_VIS / GAIN_VIS
          - b_1 * ALS_IR / GAIN_IR )
ELSE IF (ALS IR / ALS VIS) < r 2
LUX = (a 2 * ALS VIS / GAIN VIS
          - b 2 * ALS IR / GAIN IR )
ELSE IF (ALS IR / ALS VIS) < (0.95* r 3)
LUX = (a 3 * ALS VIS / GAIN VIS
          - b_3 * ALS_IR / GAIN_IR )
ELSE IF (ALS IR/ALS VIS) < (1.5 * r 3)
LUX = (2 * a_3 * ALS_VIS / GAIN_VIS
      - 1.18 * b_3 * ALS_IR / GAIN_IR)
ELSE IF (ALS IR/ALS VIS) < (2.5 * r 3)
```

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*Fig.* 18: *Typ. cover glass transmission characteristics.* 

LUX = (4 \* a\_3 \* ALS\_VIS / GAIN\_VIS - 1.33 \* b\_3 \* ALS\_IR / GAIN\_IR) Else LUX = 8 \* a\_3 \* ALS\_VIS / GAIN\_VIS LUX = LUX \* 100 ms / T\_INT\_ALS Eq. (13)

**Note 1:** the above threshold condition via  $\mathbf{r}_{_{N}}$  is valid for having equal gain setting between GAIN\_VIS and GAIN\_IR in the application. If gain is set unequal, the threshold levels  $\mathbf{r}_{_{N}}$  need to be divided by a factor of two.

**Note 2:** To achieve the necessary accuracy during this procedure it is mandatory not to change the number of decimal places or in other words not to change the accuracy of the numbers.

#### 10.2 Implementing the Illumination (Lux) Calculation: Example

Next is a *practical example* with a cover glass featuring transmission characteristics according to Fig. 18.

- 1) Measuring of the ALS data according to the setup in Fig. 16 (see Tab. 7)
- Normalization according to Eqs. (6) and (7) and data point plotting (see Tab. 7 and Fig. 17).

- In this case a three-segment linear approximation (see Fig. 17) has been chosen.
- Deriving the final constants / equations -Eqs. (10) to (12) - like previously described:

```
IF (ALS_IR / ALS_VIS) < 0.670
LUX = (11.071 * ALS VIS / GAIN VIS
      - 14.286 * ALS_IR / GAIN_IR)
ELSE IF (ALS IR / ALS VIS) < 0.746
LUX = (5.876 * ALS VIS / GAIN VIS
      - 6.536 * ALS_IR / GAIN_IR)
ELSE IF (ALS_IR/ALS_VIS) < (0.95 * 1.56)
LUX = (1.914 * ALS VIS / GAIN VIS
      - 1.225 * ALS_IR / GAIN_IR)
ELSE IF (ALS IR/ALS VIS) < (1.5 * 1.56)
LUX = (2.0 * 1.914 * ALS VIS / GAIN VIS
      - 1.18 * 1.225 * ALS_IR / GAIN_IR)
ELSE IF (ALS_IR/ALS_VIS) < (2.5 * 1.56)
LUX = (4.0 * 1.914 * ALS VIS / GAIN VIS
      - 1.33 * 1.225 * ALS_IR / GAIN_IR)
Else
LUX = 8 * 1.914 * ALS_VIS / GAIN_VIS
LUX = LUX * 100 ms / T_INT_ALS
                                 Eq. (14)
```

The typical accuracy of this implementation is around  $\pm 20\%$  for various light sources.

#### 10.3 Proximity Sensor Detection Distance behind a Dark Cover Glass

Implementing the sensor behind a dark cover glass influences directly the detection range of the sensor.

It is important to mention that a reduced IR transmission at 940 nm through a dark cover glass also reduces the maximum detection distance (compared to the case that the sensor is operated without any cover).

As light from the sensor passes the cover glass twice (on the way to the target plus on

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Cover Glass Transmission (at IR)	Corresponding Detection Distance (Approximation)				
100 % (no glass)	100 %				
90 % (clear glass)	90 %				
x %	x %				

Tab. 8: Impact of one-way cover glass (IR-) transmission on PS detection range (assuming a sufficiently large reflector size).

its way back to the sensor) it reduces the proximity signal *PS* at sensor site by ~  $T^2$  with *T* as the one way cover transmission (e.g. T = 0.9 for 90 %). For most scenarios the relationship between proximity signal *PS* and detection distance *d* is: *PS* ~  $1/d^2$  (see also Fig. 8 to 10). Combining both relations results in: *PS* ~  $T^2/d^2$ . To achieve the same sensor signal level (counts) means that the max. detection distance is reduced by the same percentage as the cover glass' one way transmission.

As a rule of thumb, an x % one way transmission loss reduces the detection range by around x % as well (compared to not using any cover glass at all). Please refer to Tab. 8 for an approximate relationship between detection distance (e.g. threshold) and cover glass IR transmission.

To compensate for, it is recommended to increase the LED current or/and lower the PS threshold level in the relevant register.

## 10.4 Zero-Distance Detection

The sensors proprietary design features zero-distance touch detection. In essence the sensor delivers enough PS counts to ensure a reliable operation. This unique feature allows for easy design-in. Typical PS counts for a human finger at zero-distance are e.g. 800 counts (finger directly on sensor at 200 mA IR-LED current) resp. around 500 counts (directly on cover glass at 200 mA IR-LED current), way above any typ. threshold setting. This is valid for human skin but not necessarily for any arbitrary reflector.

Compared to conventional proximity sensors, the SFH 7779 operates at 940 nm which features better detection of black hair.

### 10.5 Design of the Cover Glass' Aperture Opening

To ensure a fully functional design (primarily to achieve the desired level of PS crosstalkimmunity but also to achieve a certain receptive angle of the ALS) a two-hole aperture design is recommended. Compared to a single (oval) - hole design the two-hole approach delivers less (dark) ink-dependent crosstalk and improves the crosstalk-free range. Note that the SFH 7779 delivers (due to its 940 nm emitter) even less crosstalk in a single (oval) hole design compared to conventional 850 nm based products.

Please refer to Fig. 5 resp. 11 for the detector directivity and the radiation characteristics of the IR-LED (emitter).

To achieve the maximum switching distance, the recommended minimum aperture diameter of the cover glass opening depends on the airgap and can be calculated according to:

$$\emptyset \ge 2 \cdot (\Delta d + 0.45 \text{ mm}) \cdot \tan 35^\circ$$
 Eq. (15)

 $\triangle$ d is the airgap between the top surface of the SFH 7779 and the bottom of the cover glass where the aperture is located (see also Fig. 19). The maximum recommended aperture diameter is in the range of up to 2.0 mm to 1.8 mm to ensure a stable crosstalkinsensitive design, with effective multipath suppression.

However these dimensions don't consider any manufacturing tolerances.

Note that the proximity sensor alone works also with smaller apertures; but a too small aperture ( $\emptyset << 1.0$  mm) might impact the

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Fig. 19: Circular aperture design for a cover glass. The above values represent an arrangement without considering mechanical tolerances. The minimum recommended aperture diameter can be calculated to be  $\emptyset \ge 2 \cdot (\Delta d + 0.45mm) \cdot tan 35^\circ$  with  $\Delta d$  as the airgap. Performance evaluation is recommended in any case to verify the viability of the design. Note that the sensor also performs in a less than ideal environment (e.g. smaller apertures), but this might lead to a decrease in maximum detection distance. In general, to achieve crosstalk-insensitivity, OSRAM recommends limiting the airgap to below 0.5 mm (please refer to Fig. 12). Low reflective structures are recommended in the vicinity of the sensor for optimized performance.

max. detection distance and limit the ambient light sensors angular sensitivity.

The required aperture opening diameter has been minimized in order to reduce the cover glass aperture opening size required for maximum performance. This feature improves the visual impression of the mobile device by keeping the sensor invisible for users. On the other hand the sensors design ensures that a direct touch with a human hand is still detected (e.g. zero-distance detection capability).

For the typical case of an airgap of 0.2 mm OSRAM recommends to use an aperture opening of e.g. 1.6 mm. Fig. 19 illustrates the above recommendations by utilizing an  $\emptyset$  1.6 mm aperture.

A single-hole (oval) aperture design also works, but - depending on the quality of the dark ink – might result in an additional crosstalk (some counts) compared to a twohole solution. Further it is recommended to apply an IR intransparent / low reflective coating (e.g. dark black) on the bottom side of the cover glass. In general it is mandatory for an optimized crosstalk-insensitive performance that the immediate vicinity of the sensor is also low reflective (e.g. dark black). In this context OSRAM recommends to avoid the sensor close to other placing components or objects as their reflections might impair the performance of the sensor.

#### 10.6 Electrical Circuit and Layout Considerations

Fig. 20 illustrates a recommendation for implementing the SFH 7779 into a mobile phone environment.

To achieve maximum sensitivity concerning the proximity functionality it is mandatory to have a stable (battery-like) power supply. The recommendation therefore is to connect  $V_{LED}$  directly to the battery. This ensures the necessary LED current during the pulsed operation (up to 200 mA peak, depending on the actual settings of the proximity sensor's LED current). It is further



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*Fig. 20: Recommended implementation into a mobile phone environment.* 

recommended to use capacitors as close to the component as possible. Typ. values are 10  $\mu$ F at the V<sub>LED</sub> side (for up to 200 mA pulse current) and 100 nF for the V<sub>DD</sub> circuit (ASIC supply). The 10  $\mu$ F capacitor depends on the impedance of the voltage source and can e.g. be reduced if the LED pulse current is reduced to lower levels, e.g. 50 mA.

This is especially important in a *laboratory environment* as regulated power supplies often have poor pulse current capabilities.

The SCL, SDA and INT lines require pull-up resistors to the logic voltage (V<sub>IO</sub>). The limits for the logic levels are according to the l<sup>2</sup>C-bus specification (1.65 V to 2.0 V) [2]. A recommended value for R<sub>p</sub> is e.g. 10 k $\Omega$ . Please note the actual value of the pull-up resistor depends - among other issues - on the total load and communication speed of the l<sup>2</sup>C-bus.

Fig. 21 presents a reference soldering-pad design. Please refer to the SFH 7779 datasheet for the most up-to-date recommendation.

## **11. Device Handling and Cleaning**

In order to protect the semiconductor chips from environmental influences, e.g. in the soldering environment, a tape based encapsulant is used. Since this tape is very



21: Recommended soldering pad design.

elastic and soft, mechanical stress or damage to the tape should be avoided during processing/assembly. The tape must not be removed under any circumstances.

Excessive force applied to the cover (tape) can lead to a spontaneous failure of the component (damage to the contacts). To prevent damaging or puncturing the tape, the use of all types of sharp objects should be avoided both in the laboratory and factory environments.

#### Cleaning

In general, OSRAM Opto Semiconductors does not recommend a wet cleaning process for components like the SFH 7779 as the package is not hermetically sealed. Due to the open design, all kind of cleaning liquids can infiltrate the package and cause degradation or a complete failure of the component. It is also recommended to prevent penetration of organic substances from the environment which could interact with the hot surfaces of the operating chips. cleaning Ultrasonic is generally not recommended for all types of LEDs (see also the application note "Cleaning of LEDs").

As is standard for the electronic industry, OSRAM Opto Semiconductors recommends using low-residue or no-clean solder paste, so that PCB cleaning after soldering is no longer required.

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In any case, all materials and methods should be tested beforehand in order to determine whether the component will be damaged in the process.

## **12. Sample Software Code**

Below are simple C-codes which can be used to operate the SFH 7779 in connection with a microcontroller (e.g. PIC18F46J50

#### 12.1 Operating the ALS

#### 12.1.1 C-code in main program:

from Microchip). The program consists of the commented main micro C-code for the microcontroller, using the two subroutines  $12C_w_3$ : 3 write statements  $12C_w_2_r_1$ : 2 write and 1 read statement.

The main program can be implemented into a repeating loop to get the actual PS resp. ALS data or operate in interrupt mode.

sfh\_address = 0x39; // address of SFH 7779 I2C\_w\_3 (sfh\_address\*2, 0x41, 0x08); I2C\_w\_3 (sfh\_address\*2, 0x42, 0x28); // initiate ALS: 400ms rep rate, T\_int=100ms
// set ALS\_VIS=ALS\_IR GAIN = 64
// read lsb of ALS\_VIS, register 0x46 I2C\_w\_2 r\_1 (sfh\_address\*2, 0x46); Content1 = Content; (sfh\_address\*2, 0x47); // read msb of ALS\_VIS, register 0x47 (Content \* 256 + Content1); // combining LSB+MSB byte to decimal value (sfh\_address\*2, 0x48); // read lsb of ALS\_IR, register 0x48 I2C\_w\_2\_r\_1 (sfh\_address\*2, 0x47); ALS\_VIS = (Content \* 250 + Content I2C\_w 2 r\_1 (sfh\_address\*2, 0x48); Content; I2C\_w\_2\_r\_1 (sfh\_address\*2, 0x49); l (sfh\_address\*2, 0x49); // read msb of ALS\_IR, register 0x49 (Content \* 256 + Content1); // combining LSB+MSB byte to decimal value ALS IR = // Lux Calculation based on ALS Gain = 64 and ALS\_Int\_Time = 100 ms // Lux value in front of sensor, no cover glass IF  $((ALS_IR / ALS_VIS) < 0.109)$ {LUX = (1.534 \* ALS\_VIS / 64 - 3.759 \* ALS\_IR / 64) \* 1};  $\{ \text{LOX} = (1.534 \text{ ALS_VIS} / 64 - 3.759 \text{ ALS_IR} / 64) \text{ AI} \};$   $\text{ELSE IF } ((\text{ALS_IR} / \text{ALS_VIS}) < 0.429)$   $\{ \text{LUX} = (1.339 \text{ ALS_VIS} / 64 - 1.972 \text{ ALS_IR} / 64) \text{ AI} \};$   $\text{ELSE IF } ((\text{ALS_IR}/\text{ALS_VIS}) < (0.95 \text{ ALS_IR} / 64) \text{ AI} \};$   $\text{ELSE IF } ((\text{ALS_IR}/\text{ALS_VIS}) < (0.95 \text{ ALS_IR} / 64) \text{ AI} \};$   $\text{ELSE IF } ((\text{ALS_IR}/\text{ALS_VIS}) < (1.5 \text{ ALS_IR} / 64) \text{ AI} \};$   $\text{ELSE IF } ((\text{ALS_IR}/\text{ALS_VIS}) < (1.5 \text{ ALS_IR} / 64) \text{ AI} \};$   $\text{ELSE IF } ((\text{ALS_IR}/\text{ALS_VIS}) < (1.5 \text{ ALS_IR} / 64) \text{ ALS_$ ELSE IF ((ALS\_IR/ALS\_VIS) < (2.5 \* 1.45)) {LUX = (4 \* 0.701 \* ALS\_VIS / 64 - 1.33 \* 0.483 \* ALS\_IR / 64) \* 1}; Else {LUX = 8 \* 0.701 \* ALS\_VIS / 64};

#### 12.1.2 I2C\_w\_3 subroutine

void I2C\_w\_3 (unsigned char addw, unsigned char com, unsigned char daw) unsigned char var; OpenI2C (MASTER, SLEW\_ON); // Configures I2C bus module, 100 kHz transfer // setting I2C 100 kHz frequency with f osc = 16 MHz // Generates I2C bus start condition = 0x27;SSP1ADD StartI2C (); // Loop till I2C bus is idle IdleI2C (); var = WriteI2C(addw); // Microchips' Write command to write device address // var = 0: no bus error if (var == 0) write\_s++; if (var == -1) write\_c++; if (var == -2) write\_ac++; // var = -1: slave did not acknowledge write
// var=-2:write collision (bus not ready to tx) // stop further transmission if error occurred if (var < 0) goto stop; var = WriteI2C(com); // write device register address // counting of good transmissions
// counting of no acknowledge errors
// counting of write collision errors if (var == 0) write\_s++; if (var == -1) write\_c++; if (var == -2) write\_ac++; if (var < 0) goto stop;</pre>

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```
var = WriteI2C(daw); // write register content
if (var == 0) write_s++;
if (var == -1) write_c++;
if (var == -2) write_ac++;
stop:
StopI2C (); // generates I2C bus stop condition
CloseI2C (); // master I2C module disabled
```

### 12.1.3 Subroutine I2C\_w\_2\_r\_1

}

```
void I2C_w_2_r_1 (unsigned char addr, unsigned char com)
   unsigned char var;
   OpenI2C (MASTER, SLEW_ON);
   SSPADD = 0x27;
   StartI2C ();
   IdleI2C ();
   var = WriteI2C(addr);
   if (var == 0) read_s++;
if (var == -1) read_c++;
   if (var == -2) read_ac++;
if (var < 0) goto stop;</pre>
   var = WriteI2C(com);
   if (var == 0) read_s++;
   if (var == -1) read_c++;
if (var == -2) read_ac++;
   if (var < 0) goto stop;
   RestartI2C ();
                                                 // generates I2C bus restart condition
   IdleI2C ();
   var = WriteI2C(addr+1);
   if (var == 0) read_s++;
if (var == -1) read_c++;
   if (var == -2) read_ac++;
if (var < 0) goto stop;
Content = 0;
Content = ReadI2C ();</pre>
   SSPCON2bits.ACKDT = 1;
                                                 // No master Acknowledge to terminate sequence
                                                 // sending No Acknowledge bit
   SSPCON2bits.ACKEN = 1;
   PIR1bits.SSPIF = 0;
   while (SSPCON2bits.ACKEN == 1);
   PIR1bits.SSPIF = 0;
                                                 // waiting till NA causes interrupt
   stop:
   StopI2C ();
   CloseI2C ();
}
```

#### 12.2 Operating the PS

Below is a small C-code for the main program to operate the proximity sensor of the SFH 7779. The two subroutines, I2C\_w\_3 and I2C\_w2\_r1 are the same as above (see Sec. 12.1.2 and 12.1.3).

C-code for main program:

```
sfh_address = 0x39; // address of SFH 7779
I2C_w_3 (sfh_address*2, 0x41, 0x03); // initialize PS (100ms repetition rate)
I2C_w_3 (sfh_address*2, 0x42, 0x30); // run PS with 200 mA IR LED current
I2C_w_2_r_1 (sfh_address*2, 0x44); // read LSB data byte of PS, register 0x44
PS = Content;
I2C_w_2_r_1 (sfh_address*2, 0x45); // read MSB data byte of PS, register 0x45
PS = (PS + Content* 256); // combining low+high byte to decimal value
```

```
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```

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#### 12.3 Operating the ALS and PS in Interrupt Mode

The small C-code below operates the SFH 7779 in the interrupt mode. The ALS and PS are in free-running mode. The interrupt event can occur through an ALS or PS event. The interrupt event limits for ALS and PS are to be set within the program (variables: LSB\_UP, MSB\_UP, LSB\_LOW, MSB\_LOW, LSB\_Prox\_Limit\_Int\_On, MSB\_Prox\_Limit\_Int\_On, LSB\_Prox\_Limit\_Int\_Off, MSB\_Prox\_Limit\_Int\_off). After the interrupt has triggered the microcontroller the relevant sensor is determined and the ALS or PS value is read out. The calculated illumination value (1ux) assumes no cover above the sensor.

#### C-code for main program:

// General: I2C w 3 (0x39\*2, 0x41, 0x09); // ALS: 400ms repetition rate, T\_int=100ms, PS: 100ms repetition rate I2C\_w\_3 (0x39\*2, 0x42, 0x2B); // ALS gain: 64, PS current = 200mA I2C\_w\_3 (0x39\*2, 0x4A, 0x13); // set interrupt 12C\_w\_3 I2C w 3 // interrupt triggered by PS hysteresis and ALS, latched // ALS: // setting LSB of upper ALS\_VIS limit
// setting MSB of upper ALS\_VIS limit
// setting LSB of lower ALS\_VIS limit I2C\_w\_3 I2C\_w\_3 (0x39\*2, 0x4F, LSB\_UP); (0x39\*2, 0x50, MSB\_UP); (0x39\*2, 0x51, LSB\_LOW); (0x39\*2, 0x52, LSB\_LOW); I2Cw3 // setting MSB of lower ALS VIS limit I2C\_w\_3 // Prox: I2C\_w\_3 (0x39\*2, 0x4B, LSB Prox Limit Int On); // LSB for prox INT-ON limit (0x39\*2, 0x4C, MSB\_Prox\_Limit\_Int\_On); // MSB for prox INT-ON limit (0x39\*2, 0x4C, MSB\_Prox\_Limit\_Int\_Off); // LSB for prox INT-OFF limit (0x39\*2, 0x4E, MSB\_Prox\_Limit\_Int\_Off); // MSB for prox INT-OFF limit I2C w 3 // MSB for prox INT-ON limit I2C w 3 I2C\_w\_3 // Interrupt routine: // called when interrupt happened I2C\_w\_2\_r\_1 (0x39\*2, 0x4A); // reading Interrupt (Status) Register,
// Function returns register value as variable Content if ( (Content & 0x53) == 0x53) // &=bitwise AND,check whether ALS triggered interrupt
{ I2C\_w\_2\_r\_1 (0x39\*2, 0x46); // read LSB of ALS\_VIS, register 0x46 Content1 = Content; I2C\_w\_2\_r\_1 (0x39\*2, 0x47);
ALS\_VIS = (Content \* 256 + Content1);
I2C\_w\_2\_r\_1 (0x39\*2, 0x48); // read MSB of ALS\_VIS, register 0x47
// calc ALS\_VIS in decimal
// read LSB of ALS\_IR, register 0x48 Content1 = Content; I2C\_w\_2\_r\_1 (0x39\*2, 0x49); ALS\_IR = (Content \* 256 + Content1); // read MSB of ALS\_IR, register 0x49
// calc ALS\_IR in decimal // Lux Calculation based on ALS Gain = 64 and ALS Int Time = 100 ms  $\,$ // Lux value in front of sensor, no cover glass
// REFER TO EQ. (1) for the set of Instructions if ( (Content & 0x93) == 0x93) // &=bitwise AND, check whether PS triggered interrupt // read LSB of PS, register 0x44 I2C\_w\_2\_r\_1 (0x39\*2, 0x44); ContentP = Content;I2C w 2 r 1 (0x3F\*2, 0x45);
PS = Content \* 256 + ContentP; // read MSB of PS, register 0x45 } // end of interrupt routine

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# 12.4 Implementation into a Mobile Phone Environment

Below are two example flowcharts, describing how the SFH 7779 can be implemented into a microcontroller based mobile phone environment. The interrupt function allows for low-power stand-alone operation of the device.

The first flowchart illustrates a possible operation of the proximity sensor, the second flowchart relates to the operation of the ambient light sensor.

## 12.4.1 Operation of the PS

Fig. 22 illustrates the flowchart for a microcontroller based proximity-only sensing example.

The interrupt alerts the microcontroller only in case an object passes a certain distance threshold (towards the display, e.g. in a mobile phone). This allows the mobile phone to disable the touchscreen / turn-off the display illumination e.g. during a call to save battery power. The setting of a userdefined hysteresis (e.g. two threshold levels) reduces the microcontroller – sensor interaction to a minimum, thus reducing the overall power consumption.

## 12.4.2 Operation of the ALS

Fig. 23 illustrates a flowchart for a microcontroller based ambient light sensing. The SFH 7779 is in the free-running mode, which helps to minimize traffic on the I2C-bus as well as to relieve the microcontroller from unnecessary work load. This arrangement helps to save valuable battery power.

From time to time the ALS\_VIS and ALS\_IR data sets are read from the SFH 7779.

Based on the calculated ALS-ratio (= ALS\_IR / ALS\_VIS) and by applying subsequently the Eqs. according to Sec. 10.1, the "true" ambient light value (illumination) in front of the sensor can be calculated. These Eqs. need to be adapted in case of a dark cover glass with different spectral transmission properties (visible vs. IR) is used.



Fig. 22: Flowchart for a microcontroller based **proximity sensing** example.

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Fig. 23: Flowchart for a microcontroller based **ambient light sensing** example. After performing the ALS\_IR/ALS\_VIS ratio calculation the true illumination (lux) value can be directly calculated according to the Eqs. Please note that these Eqs. need to be adapted to the characteristic cover glass transmission properties (e.g. a simple gain factor to account for the attenuation if implemented behind a dark cover glass with flat transmission characteristics (visible to infrared range) or by adaption of the parameters if implemented behind dark, IR transmissive cover glasses). See Sec. 10.1 for more details.

## 13. Literature

OSRAM-OS: http://<u>www.osram-os.com</u>.
 "UM10204 I<sup>2</sup>C-bus specification and user manual" from NXP Rev. 03 – 19 June 2007

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Appendix



**Don't forget:** LED Light for you is your place to be whenever you are looking for information or worldwide partners for your LED Lighting project. www.ledlightforyou.com

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